# **Current Limiting with Comparator Circuit**



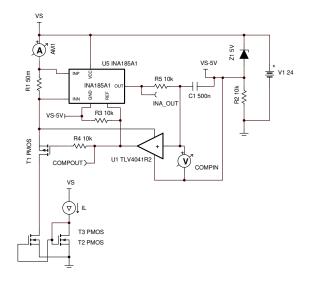
Chuck Sins

#### **Design Goals**

LOAD CURRENT (I <sub>L</sub> )	SYSTEM SUPPLY (V <sub>S</sub> )	CURRENT SENSE AMP	COMPARATOR	DUTPUT STATUS
Over Current (I <sub>OC</sub> )	Typical	Gain	Over Current	Normal Operation
200mA	24V	20V/V	V <sub>OH</sub> = V <sub>S</sub>	V <sub>OL</sub> = V <sub>S</sub> - 5V

#### **Design Description**

This high-side, current sensing solution uses a current sense amplifier, a comparator with an integrated reference, and a P-channel MOSFET to create an over-current latch circuit. When a load current greater than 200mA is detected, the circuit disconnects the system from its power source. Since the comparator drives the gate of the P-channel MOSFET and feeds the signal back into the reference pin of the current sense amplifier, the comparator output will latch (hold the gate source voltage of the P-channel MOSFET to 0V) until power to the circuit is cycled.



#### **Design Notes**

- 1. Select a precision, current sense amplifier (INA) with an external reference pin so its output voltage can be adjusted.
- 2. Select a comparator with a rail-to-rail input so its output will be valid over the entire operating voltage range of the current sense amplifier.
- 3. Select a comparator with a push-pull output stage that can drive the gate of a MOSFET and an integrated reference to optimize circuit accuracy.
- 4. Create a floating 5V supply that can power the INA and comparator.

#### **Design Steps**

 Select the value of R<sub>1</sub> so V<sub>SHUNT</sub> is at least 100x greater than the current sense amplifier input offset voltage (V<sub>OS</sub>). Note that making R<sub>6</sub> very large will improve OC detection accuracy but will reduce supply headroom and power dissipation.

$$V_{SHUNT} = (I_{OC} \times R_1) \ge 100 \times V_{OS}$$

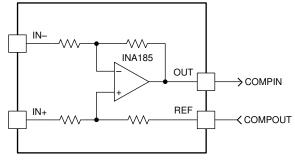
Set 
$$R_1 \ge \frac{100 \times V_{OS}}{I_{OC}} = 50 \text{m}\Omega$$
 for  $I_{OC} = 200 \text{mA}$  &  $V_{OS} = 100 \mu V$ 

2. Determine the desired gain  $(A_V)$  option for the INA based on the switching threshold of the comparator. When the load current  $(I_L)$  reaches the over-current threshold  $(I_{OC})$ , the INA output must cross the switching threshold  $(V_{TH})$  of the comparator.

$$V_{TH} = (I_{OC} \times R_1) \times A_V = 0.2V$$

Set 
$$A_V = \frac{V_{TH}}{I_{OC} \times R_1} = \frac{0.2}{0.2 \times 0.05} = 20 V/V$$
 for  $R_1 = 50 m\Omega$ 

- 3. Since many INA's and comparators have 5V operating voltage ranges, a 5V supply voltage needs to be derived from the system supply  $V_S$ . In addition, the 5V supply needs to float below  $V_S$  so the comparator output can drive the source-gate voltage of the P-channel MOSFET to 0V when an over-current condition occurs and 5V when the load current is less than  $I_{OC}$ . The method used in this circuit is a 5V zener diode with a 10 k $\Omega$  bias resistor ( $R_2$ ). Other options such as shunt regulators can also be utilized as long as proper bias current through the device is maintained.
- 4. A low pass filter is added between the INA output and the comparator input to attenuate any high frequency current spikes. It is more important to trigger the over-current latch with a delay than to falsely disconnect the system from the supply voltage. The low pass filter is derived from R<sub>5</sub> and C<sub>1</sub>. Since the switching threshold of the comparator is 0.2V, the delay is less than 1 time constant (R<sub>5</sub>×C<sub>1</sub>=5ms).
- 5. A current limiting resistor  $R_4$  is inserted between the comparator output and the gate of the P-channel MOSFET. Setting  $R_4$  to 10 k $\Omega$  reduces current spikes on the supply when the comparator output needs to charge the MOSFET gate-source capacitance as a compromise to increasing the charge time. Inserting  $R_4$  also serves the purpose of protecting the comparator output from any supply transients that can be present on the supply line.
- 6. The output of the comparator is directly connected to the REF pin of the INA in order to apply an offset to the INA's output voltage. When  $I_L < I_{OC}$ , the comparator output is low (equal to  $V_S$ -5V) and no offset is added to the INA. However, when  $I_L > I_{OC}$ , the comparator output goes high (equal to  $V_S$ ) and a 5V offset is added to the INA. This offset causes the INA output to saturate at a level equal to  $V_S$ . Since an INA output level of  $V_S$  is higher than the  $V_{TH}$  of the comparator, the comparator output will remain high. This condition is referred to as a *latched* output state since the circuit will remain in this state until power to the circuit is cycled.

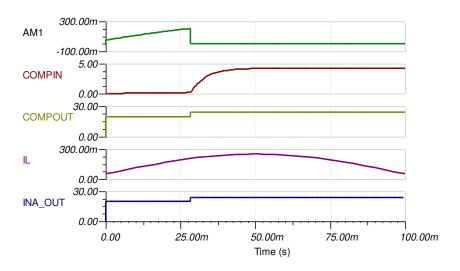


- 7. R<sub>3</sub> is added between the INA reference pin (REF) and GND (V<sub>S</sub>-5V) to ensure a proper ground path as the 5V supply ramps up to the comparator minimum operating voltage.
- 8. If a latching feature is not preferred, the comparator output can be disconnected from the current sense amplifier reference pin and R<sub>3</sub> can be replaced with a short. In this configuration, the circuit will behave as a 200mA current limiter.

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# **Design Simulations**

#### **Transient Simulation Results**



## **Design References**

Texas Instruments, SBVM944 simulation file, circuit software

## **Design Featured Comparator**

TLV4041R2			
V <sub>S</sub>	1.6V to 5.5V		
V <sub>inCM</sub>	Rail-to-rail		
V <sub>OUT</sub>	Push-Pull		
Integrated Reference	200mV ± 3mV		
IQ	2μΑ		
t <sub>PD</sub>	360ns		
TLV4041R2			

# **Design Featured Current Sense Amplifier**

INA185			
V <sub>S</sub>	2.7V to 5.5V		
V <sub>inCM</sub>	-0.2V to 26V		
Gain Options	20V/V, 50V/V, 100V/V, 200V/V		
Gain Error	0.2 %		
V <sub>os</sub>	100μV (A1), 25μV (A2, A3, and A4)		
IQ	200μΑ		
INA185			

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