

Analog Engineer's Circuit

Temperature Sensing NTC Circuit With MSP430™ Smart Analog Combo



Matthew Calvo

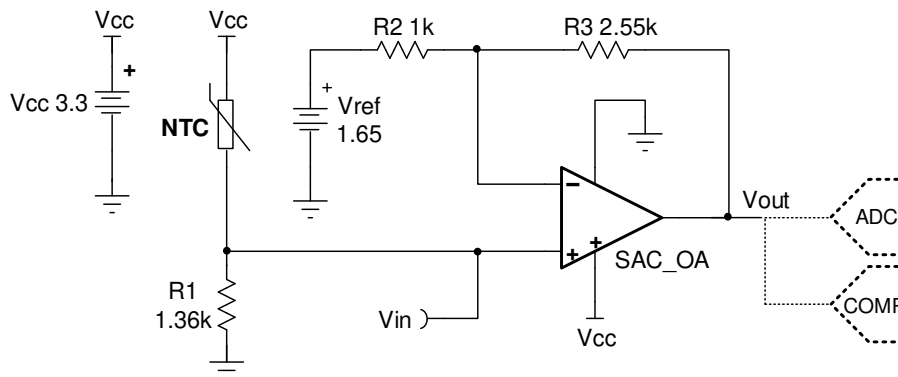
Design Goals

Temperature		Output Voltage		Supply		
T _{Min}	T _{Max}	V _{outMin}	V _{outMax}	V _{cc}	V _{ee}	V _{ref}
25°C	50°C	0.2V	3.1V	3.3V	0V	1.65V

Design Description

Some MSP430™ microcontrollers (MCUs) contain configurable integrated signal chain elements such as op-amps, DACs, and programmable gain stages. These elements make up a peripheral called the Smart Analog Combo (SAC). For information on the different types of SACs and how to leverage their configurable analog signal chain capabilities, visit [MSP430 MCUs Smart Analog Combo Training](#). To get started with your design, download the [MSP430 Temp Sense NTC Circuit Code Examples and SPICE Simulation File](#).

This temperature sensing circuit uses a resistor in series with a negative-temperature-coefficient (NTC) thermistor to form a voltage divider, which produces an output voltage that is linear over temperature. The circuit uses the MSP430FR2311 SAC_L1 op-amp in a noninverting amplifier configuration with inverting reference to offset and gain the signal, which helps to use the full ADC resolution and increase measurement accuracy. (Note: The MSP430FR2355 features four SAC_L3 peripherals which each contain a built-in DAC and PGA, providing a single-chip solution for generating V_{ref} and measuring the thermistor circuit.) The output of the integrated SAC op-amp can be sampled directly by the on-board ADC or monitored by the on-board comparator for further processing inside the MCU.



Design Notes

- The connection, Vin, is a negative temperature coefficient output voltage. To measure the output voltage of a PTC thermistor, switch the position of R₁ and the thermistor.
- V_{ref} can be generated using one of the integrated SAC_L3 DACs in the MSP430FR2355 or a voltage divider. If a voltage divider is used the equivalent resistance of the voltage divider will influence the gain of the circuit.
- Using high value resistors can degrade the phase margin of the amplifier and introduce additional noise in the circuit. It is recommended to use resistor values of approximately 10kΩ or less.

- If the solution is implemented using the MSP430FR2311, the SAC_L1 op-amp is configured in general purpose mode to measure the thermistor circuit.
- If the solution is implemented using the MSP430FR2355, one SAC_L3 peripheral is configured in DAC mode to generate the reference voltage and another is configured in general purpose mode to measure the thermistor circuit.

Design Steps

$$V_{out} = V_{cc} \times \frac{R_1}{R_{NTC} + R_1} \times \frac{R_2 + R_3}{R_2} - \frac{R_3}{R_2} \times V_{ref}$$

1. Calculate the value of R_1 to produce a linear output voltage. Use the minimum and maximum values of the NTC to obtain a range of values for R_1 .

$$R_{NTC_max} = R_{NTC} @ 25^\circ C = 2.252 \text{ k}\Omega, \quad R_{NTC_min} = R_{NTC} @ 50^\circ C = 819.7 \Omega$$

$$R_1 = \sqrt{R_{NTC} @ 25^\circ C \times R_{NTC} @ 50^\circ C} = \sqrt{2.252 \text{ k}\Omega \times 819.7 \Omega} = 1.359 \text{ k}\Omega \approx 1.36 \text{ k}\Omega$$

2. Calculate the input voltage range.

$$V_{inMin} = V_{cc} \times \frac{R_1}{R_{NTC_max} + R_1} = 3.3 \text{ V} \times \frac{1.36 \text{ k}\Omega}{2.252 \text{ k}\Omega + 1.36 \text{ k}\Omega} = 1.2418 \text{ V}$$

$$V_{inMax} = V_{cc} \times \frac{R_1}{R_{NTC_min} + R_1} = 3.3 \text{ V} \times \frac{1.36 \text{ k}\Omega}{819.7 \Omega + 1.36 \text{ k}\Omega} = 2.0582 \text{ V}$$

3. Calculate the gain required to produce the maximum output swing.

$$G_{ideal} = \frac{V_{outMax} - V_{outMin}}{V_{inMax} - V_{inMin}} = \frac{3.1 \text{ V} - 0.2 \text{ V}}{2.0582 \text{ V} - 1.2418 \text{ V}} = 3.5519 \frac{\text{V}}{\text{V}}$$

4. Select R_2 and calculate R_3 to set the gain in 3.

$$\text{Gain} = \frac{R_2 + R_3}{R_2}$$

$$R_2 = 1 \text{ k}\Omega \quad (\text{Standard value})$$

$$R_3 = R_2 \times (G_{ideal} - 1) = 1 \text{ k}\Omega \times (3.5519 \frac{\text{V}}{\text{V}} - 1) = 2.5519 \text{ k}\Omega$$

$$\text{Choose } R_3 = 2.55 \text{ k}\Omega$$

5. Calculate the actual gain based on standard values of R_2 and R_3 .

$$G_{actual} = \frac{R_2 + R_3}{R_2} = \frac{1 \text{ k}\Omega + 2.55 \text{ k}\Omega}{1 \text{ k}\Omega} = 3.55 \frac{\text{V}}{\text{V}}$$

6. Calculate the output voltage swing based on the actual gain.

$$V_{out_swing} = (V_{inMax} - V_{inMin}) \times G_{actual} = (2.0582 \text{ V} - 1.2418 \text{ V}) \times 3.55 \frac{\text{V}}{\text{V}} = 2.9 \text{ V}$$

7. Calculate the maximum output voltage when the output voltage is symmetrical around mid-supply.

$$V_{outMax} = V_{mid - supply} + \frac{V_{out_swing}}{2} = \frac{V_{cc} - V_{ee}}{2} + \frac{V_{out_swing}}{2} = \frac{3.3 \text{ V} - 0 \text{ V}}{2} + \frac{2.9 \text{ V}}{2} = 3.1 \text{ V}$$

8. Calculate the reference voltage.

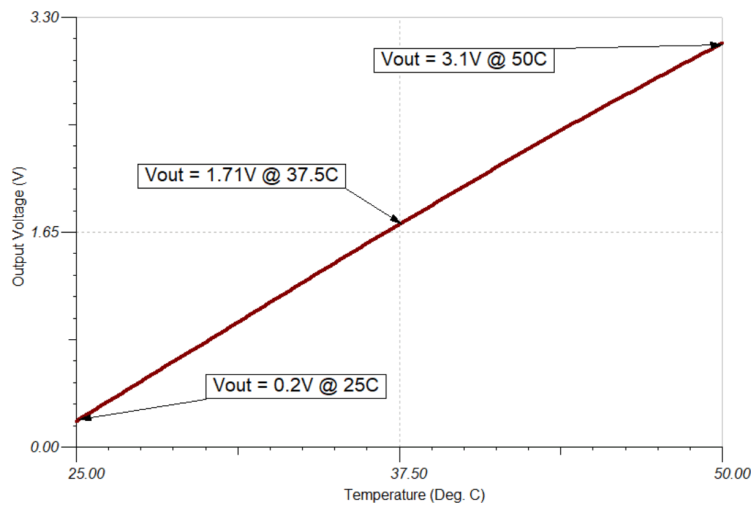
$$V_{\text{outMax}} = V_{\text{inMax}} \times G_{\text{actual}} - \frac{R_3}{R_2} \times V_{\text{ref}}$$

$$3.1 \text{ V} = 2.0582 \text{ V} \times 3.55 \frac{\text{V}}{\text{V}} - \frac{2.55 \text{ k}\Omega}{1 \text{ k}\Omega} \times V_{\text{ref}}$$

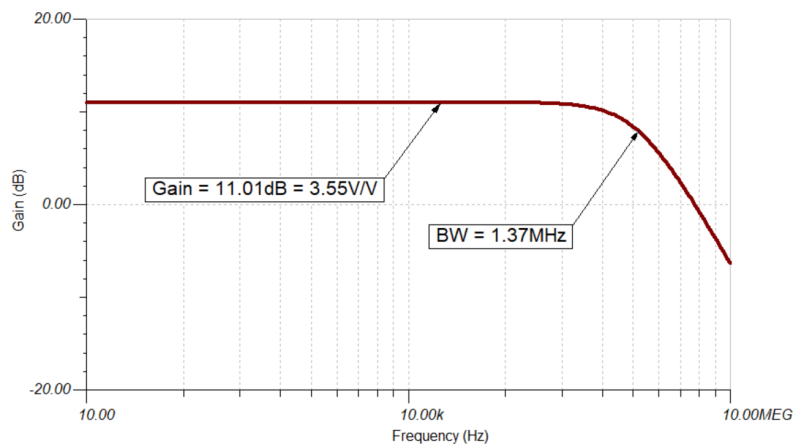
$$V_{\text{ref}} = \frac{2.0582 \text{ V} \times 3.55 \frac{\text{V}}{\text{V}} - 3.1 \text{ V}}{\frac{2.55 \text{ k}\Omega}{1 \text{ k}\Omega}} = 1.65 \text{ V}$$

Design Simulations

DC Transfer Results



AC Simulation Results



Target Applications

- [Field temperature transmitters](#)
- [Thermostats](#)
- [Thermometers](#)
- [Thermistor probes](#)
- System temperature monitor

References

Texas Instruments, [MSP430 MCUs Smart Analog Combo Training](#), video

Texas Instruments, [MSP430FR2311 TINA-TI Spice Model](#), software support



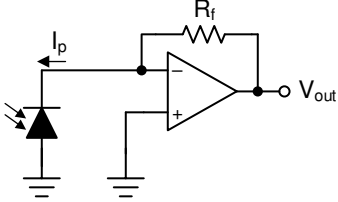
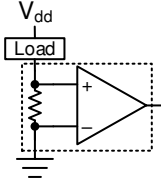
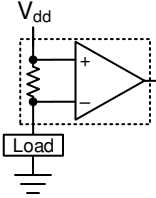
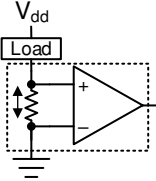

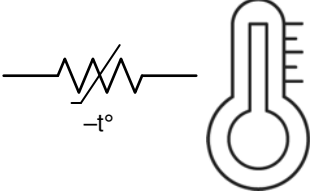
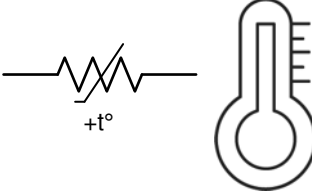
Texas Instruments, [MSP430 Temp Sense NTC Circuit Code Examples and SPICE Simulation File](#), SLAC793 design resource

Design Featured Op Amp

MSP430FRxx Smart Analog Combo		
	MSP430FR2311 SAC_L1	MSP430FR2355 SAC_L3
V_{CC}	2.0 V to 3.6 V	
V_{CM}	-0.1 V to $V_{CC} + 0.1$ V	
V_{out}	Rail-to-rail	
V_{os}	± 5 mV	
A_{OL}	100dB	
I_q	350 μ A (high-speed mode)	
	120 μ A (low-power mode)	
I_b	50pA	
UGBW	4MHz (high-speed mode)	2.8MHz (high-speed mode)
	1.4MHz (low-power mode)	1MHz (low-power mode)
SR	3V/ μ s (high-speed mode)	
	1V/ μ s (low-power mode)	
Number of channels	1	4
	MSP430FR2311	MSP430FR2355

Design Alternate Op Amp

MSP430FR2311 Transimpedance Amplifier	
V_{CC}	2.0V to 3.6V
V_{CM}	-0.1V to $V_{CC}/2$ V
V_{out}	Rail-to-rail
V_{os}	± 5 mV
A_{OL}	100dB
I_q	350 μ A (high-speed mode)
	120 μ A (low-power mode)
I_b	5pA (TSSOP-16 with OA-dedicated pin input)
	50pA (TSSOP-20 and VQFN-16)
UGBW	5MHz (high-speed mode)
	1.8MHz (low-power mode)
SR	4V/ μ s (high-speed mode)
	1V/ μ s (low-power mode)
Number of channels	1
	MSP430FR2311

<p>Low-noise and long-range PIR sensor conditioner circuit</p> 	<p>Bridge amplifier circuit</p> 	<p>Transimpedance amplifier circuit</p> 
<p>Single-supply, low-side, unidirectional current-sensing circuit</p> 	<p>High-side current sensing with discrete difference amplifier circuit</p> 	<p>Low-side, bidirectional current-sensing circuit</p> 
<p>Half-wave rectifier circuit</p> 	<p>Temperature sensing with NTC thermistor circuit</p> 	<p>Temperature sensing with PTC thermistor circuit</p> 

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Revision History

NOTE: Page numbers for previous revisions may differ from page numbers in the current version.

Changes from Revision C (March 2020) to Revision D (September 2024)	Page
• Updated the format for tables, figures, and cross-references throughout the document	1

Changes from Revision B (October 2019) to Revision C (March 2020)	Page
• Added <i>Related MSP430 Circuits</i> section.....	1

Changes from Revision A (September 2019) to Revision B (October 2019)	Page
• Updated the first paragraph in <i>Design Description</i>	1

Changes from Revision * (August 2019) to Revision A (September 2019)	Page
• Updated the link to the example files in References.....	1

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