

# ATL431LI-Q1/ATL432LI-Q1 高帯域幅、低 $I_Q$ のプログラム可能なシャント・レギュレータ

## 1 特長

- 車載アプリケーション用に認定済み
- 下記内容で AEC-Q100 認定済み
  - デバイス温度グレード 1: 動作時周囲温度  $-40^{\circ}\text{C} \sim +125^{\circ}\text{C}$
- $25^{\circ}\text{C}$ での基準電圧の許容公差
  - 0.5% (B グレード)
  - 1% (A グレード)
- 出力電圧の最小値: 2.5V (標準値)
- 可変出力電圧:  $V_{\text{ref}} \sim 36\text{V}$
- $-40^{\circ}\text{C} \sim +125^{\circ}\text{C}$ で動作
- 最大温度ドリフト: 27mV
- 出カインピーダンス:  $0.3\Omega$  (標準値)
- シンク電流能力
  - $I_{\text{min}} = 0.08\text{mA}$  (最大値)
  - $I_{\text{KA}} = 15\text{mA}$  (最大値)
- 基準入力電流  $I_{\text{REF}}: 0.4\mu\text{A}$  (最大値)
- 全温度範囲にわたる基準入力電流の偏差、 $I_{\text{I(dev)}}: 0.3\mu\text{A}$  (最大値)

## 2 アプリケーション

- インバータおよびモータ制御
- DC/DC コンバータ
- LED ライティング
- オンボード充電器 (OBC)
- インフォテインメント / クラスタ

## 3 概要

ATL43xLI-Q1 は 3 端子の可変シャント・レギュレータで、該当する車載、商業、軍事用の温度範囲全体にわたって熱的な安定性が規定されています。出力電圧は、2 つの外付け抵抗を使用して、 $V_{\text{ref}}$  (約 2.5V) から 36V までの範囲で任意の値に設定できます。このデバイスの出カインピーダンスは  $0.3\Omega$  (標準値) です。このデバイスは、アクティブ出力回路による非常に鋭い起動特性を備えているため、オンボード・レギュレーション、可変電源、スイッチング電源などの多くの用途でツェナー・ダイオードの優れた代替品となります。このデバイスは TL431LI-Q1 および TL432LI-Q1 とピン互換の代替品であり、最小動作電流が小さいため、システムの消費電力削減に役立ちます。ATL432LI-Q1 の機能と電氣的仕様は ATL431LI-Q1 と完全に同じですが、DBZ パッケージのピン配置が異なります。

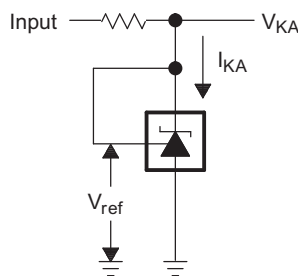
ATL431LI-Q1 は、初期公差 ( $25^{\circ}\text{C}$  時) が 0.5% の B グレードと、1% の A グレードの 2 つのグレードで供給されており、温度に対する出力ドリフトが小さいため、温度範囲全体にわたって優れた安定性が得られます。

### 製品情報<sup>(1)</sup>

型番	パッケージ(ピン)	本体サイズ(公称)
ATL43xLI	SOT-23 (3)	2.90mm×1.30mm

(1) 提供されているすべてのパッケージについては、巻末の注文情報を参照してください。

概略回路図



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## 4 改訂履歴

資料番号末尾の英字は改訂を表しています。その改訂履歴は英語版に準じています。

### 2019年5月発行のものから更新

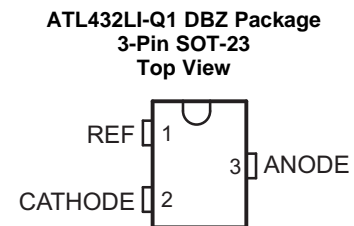
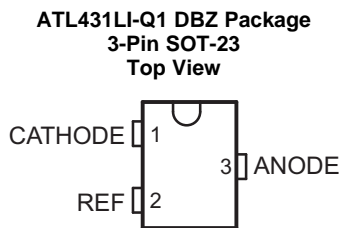
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•	デバイスのステータスを「事前情報」から「量産データ」に変更	1
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## 5 Device Comparison Table

DEVICE PINOUT	INITIAL ACCURACY	OPERATING FREE-AIR TEMPERATURE (T <sub>A</sub> )
ATL431LI-Q1 ATL432LI-Q1	A: 1% B: 0.5%	Q: -40°C to 125°C

## 6 Pin Configuration and Functions



### Pin Functions

NAME	PIN		TYPE	DESCRIPTION
	ATL431LI-Q1	ATL432LI-Q1		
	DBZ	DBZ		
ANODE	3	3	O	Common pin, normally connected to ground
CATHODE	1	2	I/O	Shunt Current/Voltage input
REF	2	1	I	Threshold relative to common anode

## 7 Specifications

### 7.1 Absolute Maximum Ratings

over operating free-air temperature range (unless otherwise noted)<sup>(1)</sup>

		MIN	MAX	UNIT
V <sub>KA</sub>	Cathode Voltage <sup>(2)</sup>		37	V
I <sub>KA</sub>	Continuous Cathode Current Range	-10	18	mA
I <sub>I(ref)</sub>	Reference Input Current	-5	10	mA
T <sub>J</sub>	Operating Junction Temperature Range	-40	150	C
T <sub>stg</sub>	Storage Temperature Range	-65	150	C

- (1) Stresses beyond those listed under *Absolute Maximum Ratings* may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under *Recommended Operating Conditions*. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
- (2) All voltage values are with respect to ANODE, unless otherwise noted.

### 7.2 ESD Ratings

			VALUE	UNIT
V <sub>(ESD)</sub>	Electrostatic discharge	Human body model (HBM), per AEC Q100-002 <sup>(1)</sup>	±4000	V
		Charged-device model (CDM), per AEC Q100-011	±1000	

- (1) AEC Q100-002 indicates that HBM stressing shall be in accordance with the ANSI/ESDA/JEDEC JS-001 specification

### 7.3 Recommended Operating Conditions

			MIN	MAX	UNIT
V <sub>KA</sub>	Cathode Voltage		V <sub>REF</sub>	36	V
I <sub>KA</sub>	Continuous Cathode Current Range		0.08	15	mA
T <sub>A</sub>	Operating Free-Air Temperature <sup>(1)</sup>	ATL43xLIxQ	-40	125	C

- (1) Maximum power dissipation is a function of T<sub>J(max)</sub>, θ<sub>JA</sub>, and T<sub>A</sub>. The maximum allowable power dissipation at any allowable ambient temperature is P<sub>D</sub> = (T<sub>J(max)</sub> - T<sub>A</sub>)/θ<sub>JA</sub>. Operating at the absolute maximum T<sub>J</sub> can affect reliability. See the [Semiconductor and IC Package Thermal Metrics Application Report](#) for more information.

### 7.4 Thermal Information

THERMAL METRIC <sup>(1)</sup>		ATL43xLI	UNIT
		DBZ	
		3 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	371.7	C/W
R <sub>θJC(top)</sub>	Junction-to-case (top) thermal resistance	145.9	C/W
R <sub>θJB</sub>	Junction-to-board thermal resistance	104.7	C/W
ψ <sub>JT</sub>	Junction-to-top characterization parameter	23.9	C/W
ψ <sub>JB</sub>	Junction-to-board characterization parameter	102.9	C/W

- (1) For more information about traditional and new thermal metrics, see the [Semiconductor and IC Package Thermal Metrics Application Report](#).

## 7.5 Electrical Characteristics

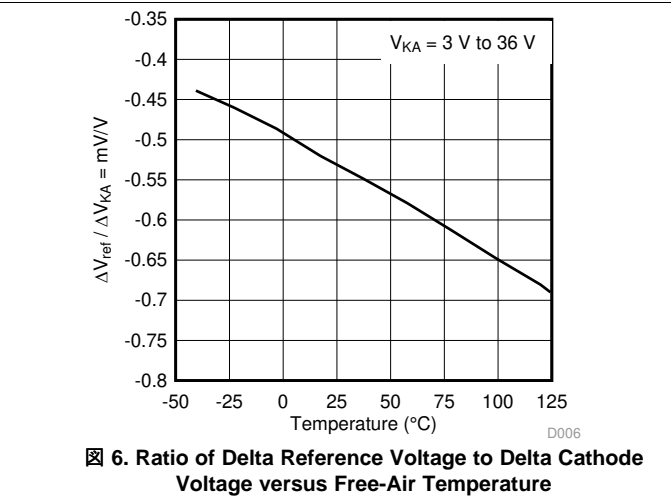
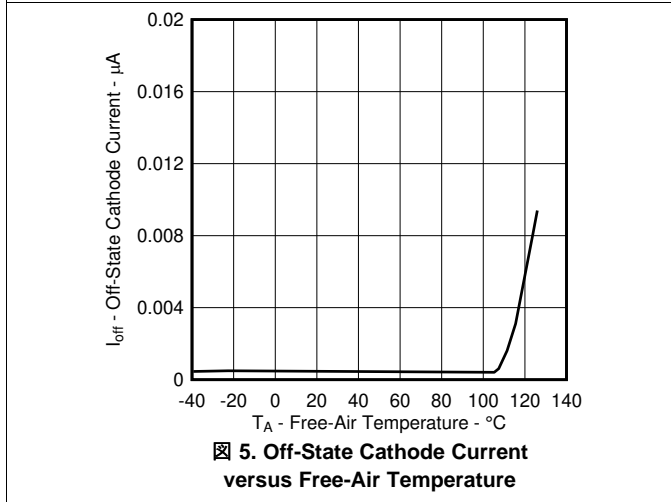
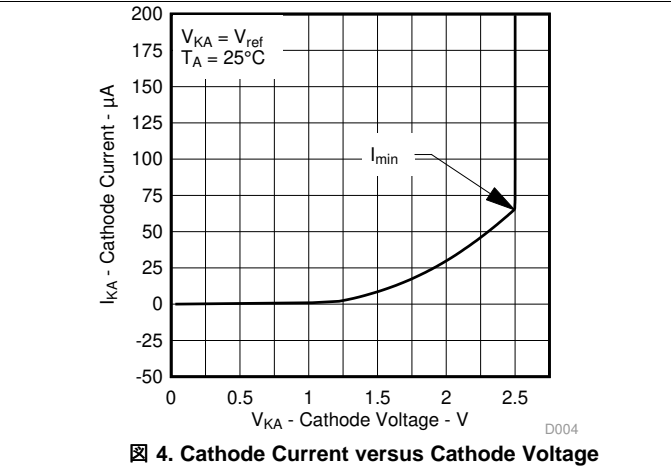
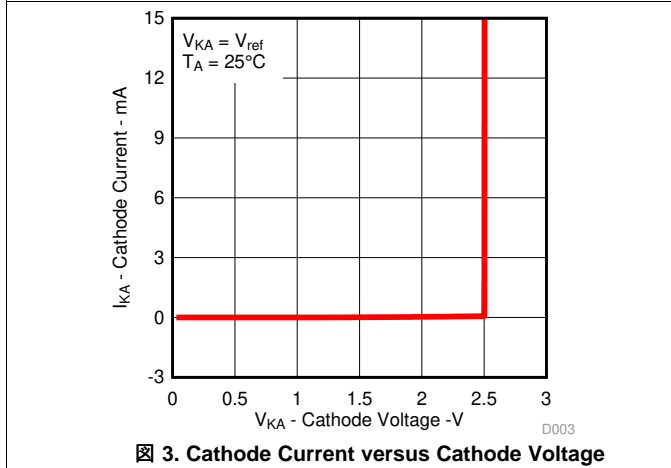
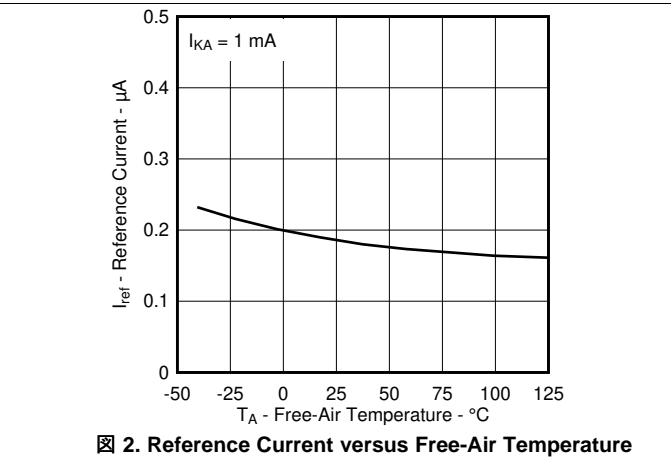
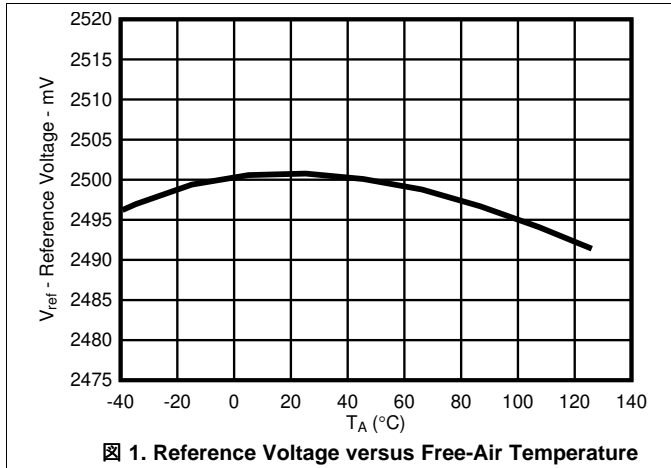
over recommended operating conditions,  $T_A = 25^\circ\text{C}$  (unless otherwise noted)

PARAMETER		TEST CIRCUIT	TEST CONDITIONS	MIN	TYP	MAX	UNIT	
$V_{\text{REF}}$	Reference Voltage	See <a href="#">17</a>	$V_{\text{KA}} = V_{\text{ref}}, I_{\text{KA}} = 1 \text{ mA}$	ATL43xLIAx devices	2475	2500	2525	mV
				ATL43xLIBx devices	2487	2500	2512	mV
$V_{\text{I(dev)}}$	Deviation of reference input voltage over full temperature range <sup>(1)</sup>	See <a href="#">17</a>	$V_{\text{KA}} = V_{\text{ref}}, I_{\text{KA}} = 1 \text{ mA}$		10	27	mV	
$\frac{\Delta V_{\text{ref}}}{\Delta V_{\text{KA}}}$	Ratio of change in reference voltage to the change in cathode voltage	See <a href="#">18</a>	$I_{\text{KA}} = 1 \text{ mA}$	$\Delta V_{\text{KA}} = 10 \text{ V} - V_{\text{ref}}$	-1.4	-2.7	mV/V	
				$\Delta V_{\text{KA}} = 36 \text{ V} - 10 \text{ V}$	-1	-2	mV/V	
$I_{\text{ref}}$	Reference Input Current	See <a href="#">18</a>	$I_{\text{KA}} = 1 \text{ mA}, R1 = 10\text{k}\Omega, R2 = \infty$		0.2	0.4	$\mu\text{A}$	
$I_{\text{I(dev)}}$	Deviation of reference input current over full temperature range <sup>(1)</sup>	See <a href="#">18</a>	$I_{\text{KA}} = 1 \text{ mA}, R1 = 10\text{k}\Omega, R2 = \infty$		0.1	0.3	$\mu\text{A}$	
$I_{\text{min}}$	Minimum cathode current for regulation	See <a href="#">17</a>	$V_{\text{KA}} = V_{\text{ref}}$		65	80	$\mu\text{A}$	
$I_{\text{off}}$	Off-state cathode current	See <a href="#">19</a>	$V_{\text{KA}} = 36 \text{ V}, V_{\text{ref}} = 0$		0.1	1	$\mu\text{A}$	
$ Z_{\text{KA}} $	Dynamic Impedance <sup>(2)</sup>	See <a href="#">17</a>	$V_{\text{KA}} = V_{\text{ref}}, I_{\text{KA}} = 1 \text{ mA to } 15 \text{ mA}$		0.65	0.75	$\Omega$	

- (1) The deviation parameters  $V_{\text{I(dev)}}$  and  $I_{\text{I(dev)}}$  are defined as the differences between the maximum and minimum values obtained over the rated temperature range. For more details on  $V_{\text{I(dev)}}$  and how it relates to the average temperature coefficient, see the [Temperature Coefficient](#) section.
- (2) The dynamic impedance is defined by  $|Z_{\text{KA}}| = \Delta V_{\text{KA}} / \Delta I_{\text{KA}}$ . For more details on  $|Z_{\text{KA}}|$  and how it relates to  $V_{\text{out}}$ , see the [Temperature Coefficient](#) section.

## 7.6 Typical Characteristics

Data at high and low temperatures are applicable only within the recommended operating free-air temperature ranges of the various devices.



Typical Characteristics (continued)

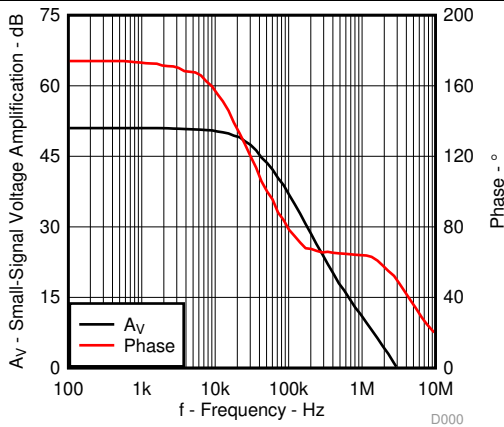


Fig. 7. Small-Signal Voltage Amplification versus Frequency

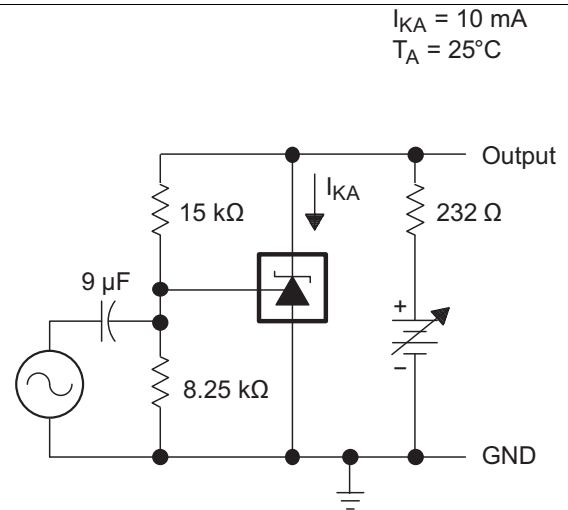


Fig. 8. Test Circuit for Voltage Amplification

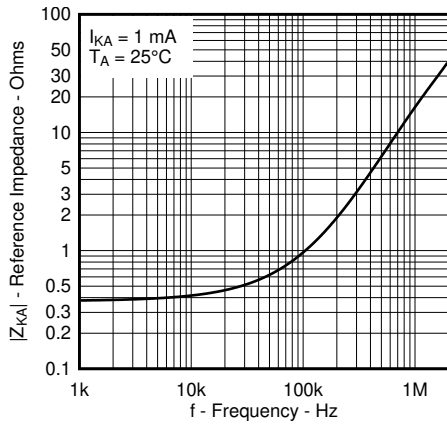


Fig. 9. Reference Impedance versus Frequency

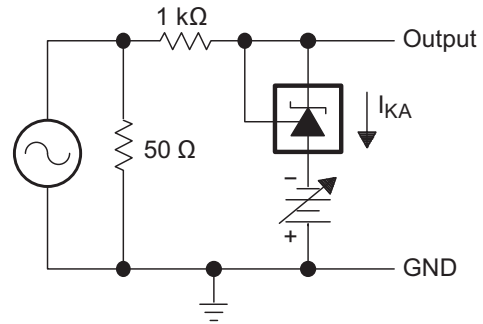


Fig. 10. Test Circuit for Reference Impedance

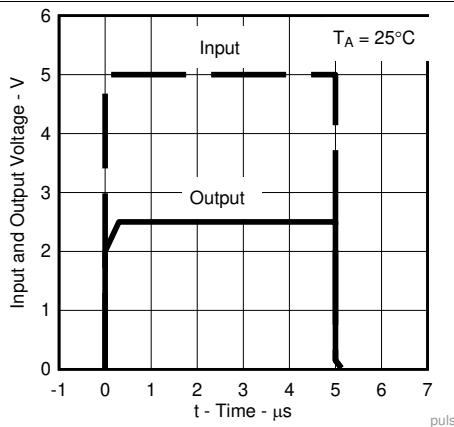


Fig. 11. Pulse Response

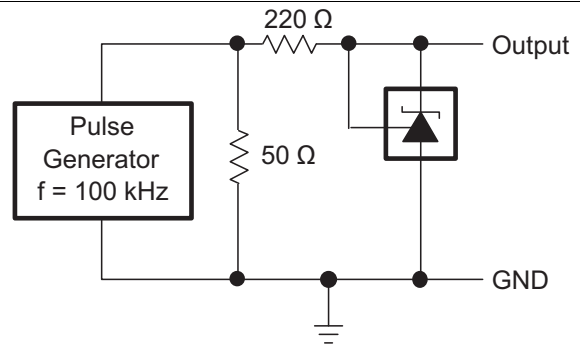
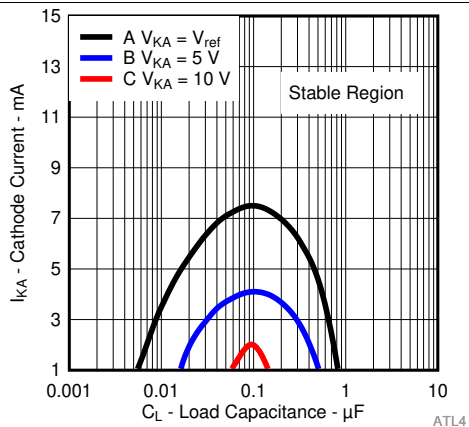


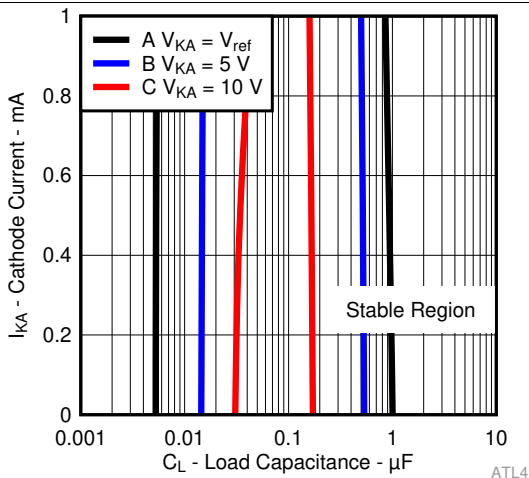
Fig. 12. Test Circuit for Pulse Response

Typical Characteristics (continued)



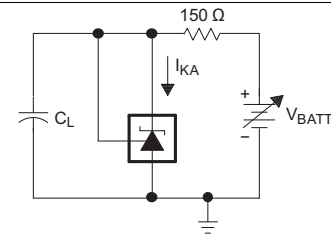
The areas under the curves represent conditions that may cause the device to oscillate. For curves B and C, R2 and V+ are adjusted to establish the initial  $V_{KA}$  and  $I_{KA}$  conditions, with  $C_L = 0$ .  $V_{BATT}$  and  $C_L$  then are adjusted to determine the ranges of stability.

Fig 13. Stability Boundary Conditions for All ATL431LI-Q1, ATL432LI-Q1 Devices Above 1 mA

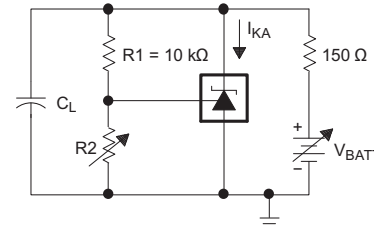


The areas in-between the curves represent conditions that may cause the device to oscillate. For curves B and C, R2 and V+ are adjusted to establish the initial  $V_{KA}$  and  $I_{KA}$  conditions, with  $C_L = 0$ .  $V_{BATT}$  and  $C_L$  then are adjusted to determine the ranges of stability.

Fig 15. Stability Boundary Conditions for All ATL431LI-Q1, ATL432LI-Q1 Devices Below 1 mA

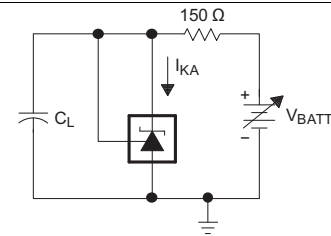


TEST CIRCUIT FOR CURVE A

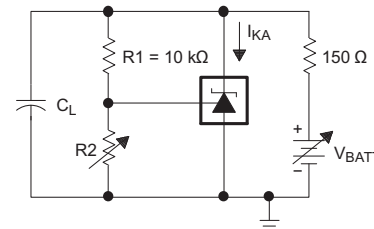


TEST CIRCUIT FOR CURVES B, C, AND D

Fig 14. Test Circuit for Stability Boundary Conditions



TEST CIRCUIT FOR CURVE A



TEST CIRCUIT FOR CURVES B, C, AND D

Fig 16. Test Circuit for Stability Boundary Conditions



## 8 Parameter Measurement Information

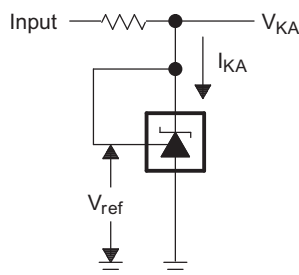


Figure 17. Test Circuit for  $V_{KA} = V_{ref}$

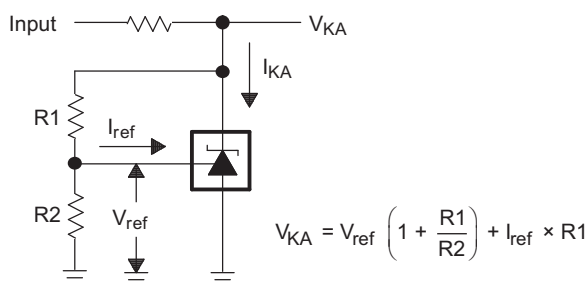


Figure 18. Test Circuit for  $V_{KA} > V_{ref}$

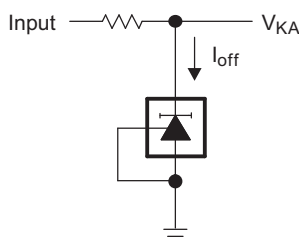


Figure 19. Test Circuit for  $I_{off}$

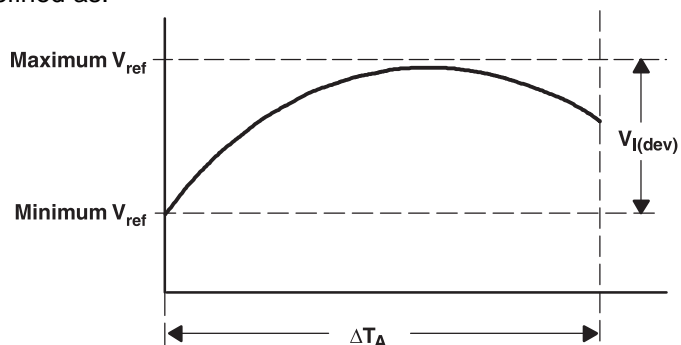
### 8.1 Temperature Coefficient

The deviation of the reference voltage,  $V_{ref}$ , over the full temperature range is known as  $V_{I(dev)}$ . The parameter of  $V_{I(dev)}$  can be used to find the temperature coefficient of the device. The average full-range temperature coefficient of the reference input voltage,  $\alpha_{V_{ref}}$ , is defined as:

$$\left| \alpha_{V_{ref}} \right| \left( \frac{\text{ppm}}{\text{°C}} \right) = \frac{\left( \frac{V_{I(dev)}}{V_{ref \text{ at } 25 \text{ °C}}} \right) \times 10^6}{\Delta T_A}$$

where:

$\Delta T_A$  is the rated operating temperature range of the device.



$\alpha_{V_{ref}}$  is positive or negative, depending on whether minimum  $V_{ref}$  or maximum  $V_{ref}$ , respectively, occurs at the lower temperature. The full-range temperature coefficient is an average and, therefore, any subsection of the rated operating temperature range can yield a value that is greater or less than the average. For more details on temperature coefficient, refer to the [Voltage Reference Selection Basics White Paper](#).

## 8.2 Dynamic Impedance

The dynamic impedance is defined as:  $|Z_{KA}| = \frac{\Delta V_{KA}}{\Delta I_{KA}}$ . When the device is operating with two external resistors (see [Figure 18](#)), the total dynamic impedance of the circuit is given by:  $|z'| = \frac{\Delta V}{\Delta I}$ , which is approximately equal to  $|Z_{KA}| \left(1 + \frac{R1}{R2}\right)$ .

The  $V_{KA}$  of the ATL431LI-Q1 can be affected by the dynamic impedance. The ATL431LI-Q1 test current  $I_{test}$  for  $V_{KA}$  is specified in the [Electrical Characteristics](#). Any deviation from  $I_{test}$  can cause deviation on the output  $V_{KA}$ . [Figure 20](#) shows the effect of the dynamic impedance on the  $V_{KA}$ .

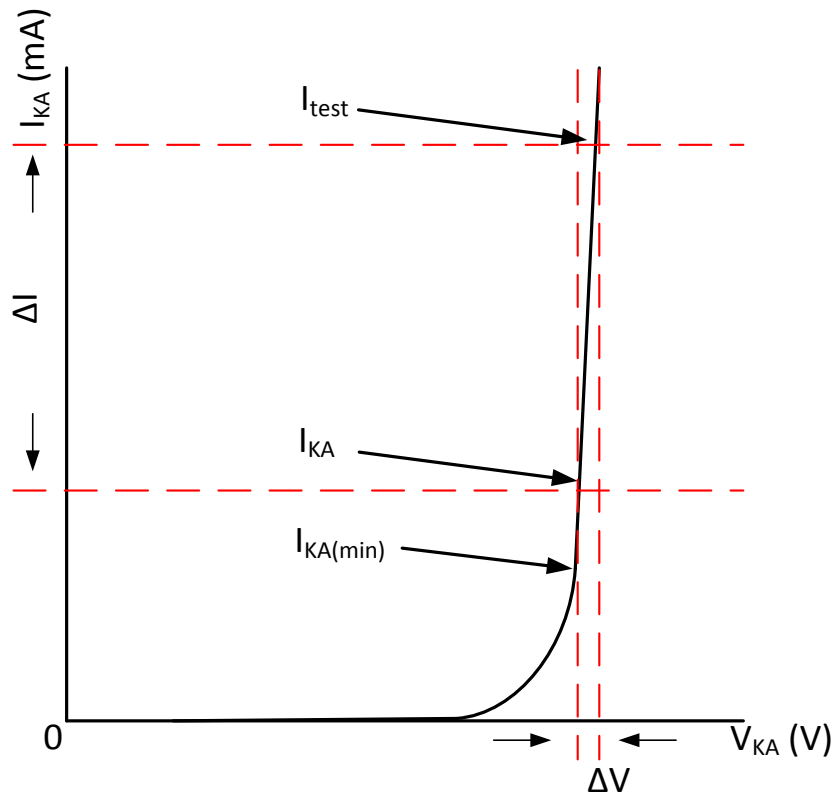


Figure 20. Dynamic Impedance

## 9 Detailed Description

### 9.1 Overview

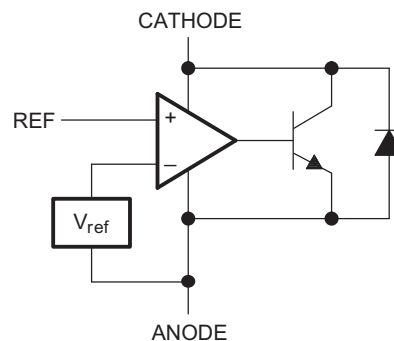
This standard device has proven ubiquity and versatility across a wide range of applications, ranging from power to signal path. This is due to its key components containing an accurate voltage reference and op amp, which are very fundamental analog building blocks. The ATL431LI-Q1 is used in conjunction with the key components to behave as the following:

- Single voltage reference
- Error amplifier
- Voltage clamp
- Comparator with integrated reference

ATL431LI-Q1 can be operated and adjusted to cathode voltages from 2.5 V to 36 V, making this part optimal for a wide range of end equipments in industrial, auto, telecom, and computing. For this device to behave as a shunt regulator or error amplifier,  $>80 \mu\text{A}$  ( $I_{\text{min}}$ (maximum)) must be supplied in to the cathode pin. Under this condition, feedback can be applied from the Cathode and Ref pins to create a replica of the internal reference voltage.

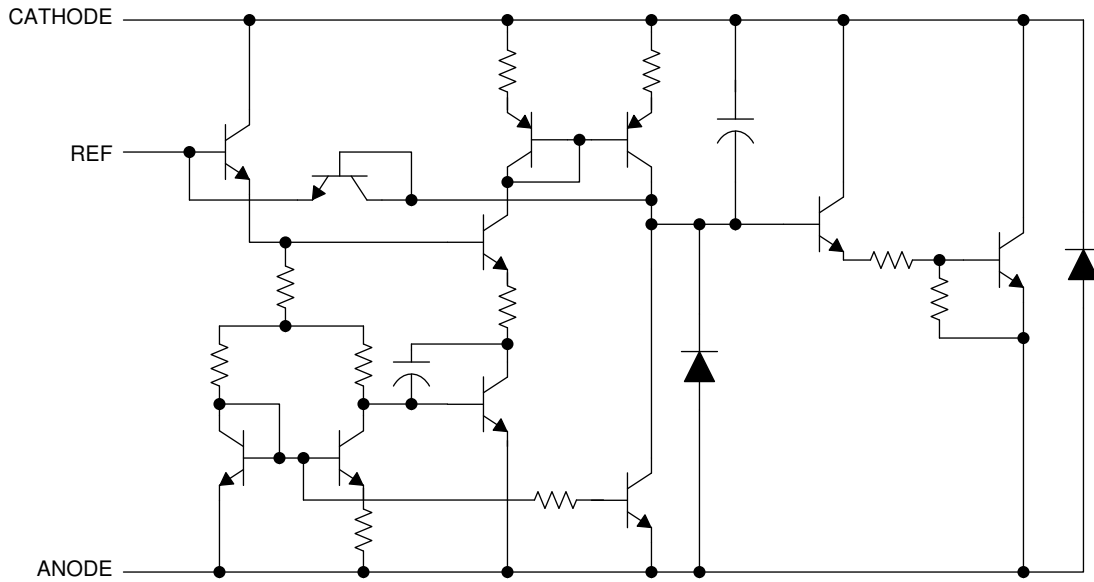
Various reference voltage options can be purchased with initial tolerances (at 25°C) of 0.5% and 1%. These reference options are denoted by B (0.5%) and A (1.0%) after the ATL431LI-Q1 or ATL432LI-Q1. ATL431LI-Q1 and ATL432LI-Q1 are both functionally the same, but have different pinout options. The ATL43xLI-Q1 devices are characterized for operation from  $-40^{\circ}\text{C}$  to  $+125^{\circ}\text{C}$ .

### 9.2 Functional Block Diagram



☒ 21. Equivalent Schematic

**Functional Block Diagram (continued)**



⊠ 22. Detailed Schematic

### 9.3 Feature Description

The ATL431LI-Q1 consists of an internal reference and amplifier that outputs a sink current based on the difference between the reference pin and the virtual internal pin. The sink current is produced by the internal Darlington pair, shown in [Figure 21](#). A Darlington pair is used for this device to be able to sink a maximum current of 15 mA.

When operated with enough voltage headroom ( $\geq 2.5$  V) and cathode current ( $I_{KA}$ ), the ATL431LI-Q1 forces the reference pin to 2.5 V. However, the reference pin cannot be left floating, as it needs  $I_{REF} \geq 0.4$   $\mu$ A (see the [Specifications](#)). This is because the reference pin is driven into an NPN, which needs base current to operate properly.

When feedback is applied from the Cathode and Reference pins, the ATL431LI-Q1 behaves as a Zener diode, regulating to a constant voltage dependent on current being supplied into the cathode. This is due to the internal amplifier and reference entering the proper operating regions. The same amount of current needed in the above feedback situation must be applied to this device in open loop, servo, or error amplifying implementations for it to be in the proper linear region giving ATL431LI-Q1 enough gain.

Unlike many linear regulators, ATL431LI-Q1 is internally compensated to be stable without an output capacitor between the cathode and anode. However, if it is desired to use an output capacitor [Figure 13](#) can be used as a guide to assist in choosing the correct capacitor to maintain stability.

### 9.4 Device Functional Modes

#### 9.4.1 Open Loop (Comparator)

When the cathode/output voltage or current of ATL431LI-Q1 is not being fed back to the reference/input pin in any form, this device is operating in open loop. With proper cathode current ( $I_{KA}$ ) applied to this device, the ATL431LI-Q1 has the characteristics shown in [Figure 21](#). With such high gain in this configuration, the ATL431LI-Q1 is typically used as a comparator. With the reference integrated makes ATL431LI-Q1 the preferred choice when users are trying to monitor a certain level of a single signal.

#### 9.4.2 Closed Loop

When the cathode/output voltage or current of the ATL431LI-Q1 is being fed back to the reference/input pin in any form, this device is operating in closed loop. The majority of applications involving ATL431LI-Q1 use it in this manner to regulate a fixed voltage or current. The feedback enables this device to behave as an error amplifier, computing a portion of the output voltage and adjusting it to maintain the desired regulation. This is done by relating the output voltage back to the reference pin in a manner to make it equal to the internal reference voltage, which can be accomplished via resistive or direct feedback.

## 10 Applications and Implementation

### 注

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

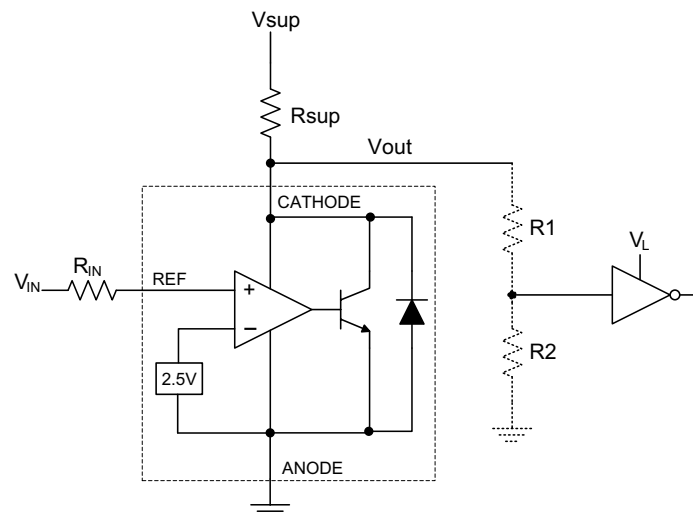
### 10.1 Application Information

As this device has many applications and setups, there are many situations that this data sheet cannot characterize in detail. The linked application note will help the designer make the best choices when using this part.

[Setting the Shunt Voltage on an Adjustable Shunt Regulator Application Note](#) assists with setting the shunt voltage to achieve optimum accuracy for this device.

### 10.2 Typical Applications

#### 10.2.1 Comparator With Integrated Reference



☒ 23. Comparator Application Schematic

## Typical Applications (continued)

### 10.2.2 Design Requirements

For this design example, use the parameters listed in [表 1](#) as the input parameters.

**表 1. Design Parameters**

DESIGN PARAMETER	EXAMPLE VALUE
Input Voltage Range	0 V to 5 V
Input Resistance	10 k $\Omega$
Supply Voltage	24 V
Cathode Current ( $I_K$ )	5 mA
Output Voltage Level	$\sim 2\text{ V} - V_{\text{SUP}}$
Logic Input Thresholds $V_{\text{IH}}/V_{\text{IL}}$	$V_L$

### 10.2.3 Detailed Design Procedure

When using the ATL431LI-Q1 as a comparator with reference, determine the following:

- Input voltage range
- Reference voltage accuracy
- Output logic input high and low level thresholds
- Current source resistance

#### 10.2.3.1 Basic Operation

In the configuration shown in [图 23](#), the ATL431LI-Q1 behaves as a comparator, comparing the  $V_{\text{REF}}$  pin voltage to the internal virtual reference voltage. When provided a proper cathode current ( $I_K$ ), ATL431LI-Q1 has enough open-loop gain to provide a quick response. This can be seen in [图 24](#) where the  $R_{\text{SUP}} = 10\text{ k}\Omega$  ( $I_{\text{KA}} = 500\text{ }\mu\text{A}$ ) situation responds much slower than  $R_{\text{SUP}} = 1\text{ k}\Omega$  ( $I_{\text{KA}} = 5\text{ mA}$ ). With the ATL431LI-Q1 max operating current ( $I_{\text{MIN}}$ ) being 1 mA, operation below that can result in low gain, leading to a slow response.

##### 10.2.3.1.1 Overdrive

Slow or inaccurate responses can also occur when the reference pin is not provided enough overdrive voltage. This is the amount of voltage that is higher than the internal virtual reference. The internal virtual reference voltage is within the range of  $2.5\text{ V} \pm(0.5\% \text{ or } 1.0\%)$  depending on which version is being used. The more overdrive voltage provided, the faster the ATL431LI-Q1 will respond.

For applications where ATL431LI-Q1 is being used as a comparator, it is best to set the trip point to greater than the positive expected error (that is +1.0% for the A version). For fast response, setting the trip point to >10% of the internal  $V_{\text{REF}}$  suffices.

For minimal voltage drop or difference from  $V_{\text{in}}$  to the ref pin, TI recommends to use an input resistor <10 k $\Omega$  to provide  $I_{\text{ref}}$ .

### 10.2.3.2 Output Voltage and Logic Input Level

For ATL431LI-Q1 to properly be used as a comparator, the logic output must be readable by the receiving logic device. This is accomplished by knowing the input high and low level threshold voltage levels, typically denoted by  $V_{IH}$  and  $V_{IL}$ .

As seen in [Figure 24](#), the output low level voltage of the ATL431LI-Q1 in open-loop/comparator mode is approximately 2 V, which is typically sufficient for 5 V supplied logic. However, this does not work for 3.3 V and 1.8 V supplied logic. To accommodate this, a resistive divider can be tied to the output to attenuate the output voltage to a voltage legible to the receiving low voltage logic device.

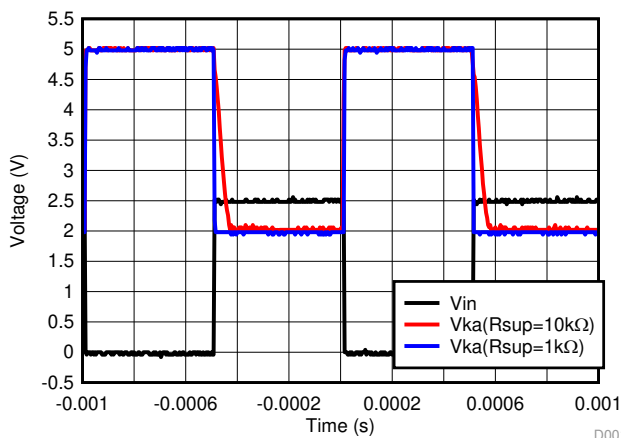
The output high voltage of the ATL431 is equal to  $V_{SUP}$  due to ATL431LI-Q1 being open-collector. If  $V_{SUP}$  is much higher than the maximum input voltage tolerance of the receiving logic, the output must be attenuated to accommodate the reliability of the outgoing logic.

When using a resistive divider on the output, make sure the sum of the resistive divider ( $R_1$  and  $R_2$  in [Figure 23](#)) is much greater than  $R_{SUP}$  to not interfere with the ability of the ATL431LI-Q1 to pull close to  $V_{SUP}$  when turning off.

#### 10.2.3.2.1 Input Resistance

The ATL431LI-Q1 requires an input resistance in this application to source the reference current ( $I_{REF}$ ) needed from this device to be in the proper operating regions while turning on. The actual voltage seen at the ref pin is  $V_{REF} = V_{IN} - I_{REF} \times R_{IN}$  because  $I_{REF}$  can be as high as 4  $\mu$ A. TI recommends to use a resistance small enough that mitigates the error that  $I_{REF}$  creates from  $V_{IN}$ .

### 10.2.4 Application Curves



**Figure 24. Output Response With Various Cathode Currents**



## 10.2.5 Precision LED Lighting Current Sink Regulator

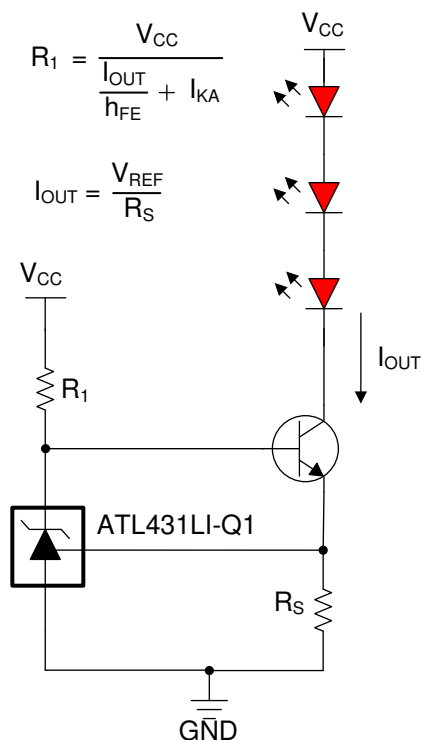


图 25. LED Lighting Current Sink Regulator

### 10.2.5.1 Design Requirements

For this design example, use the parameters listed in 表 1 as the input parameters.

表 2. Design Parameters

DESIGN PARAMETER	EXAMPLE VALUE
Supply Voltage ( $V_{(BATT)}$ )	5 V
Sink Current ( $I_O$ )	100 mA
Cathode Current ( $I_k$ )	5 mA

### 10.2.5.2 Detailed Design Procedure

When using the ATL43xLI-Q1 as a constant current sink, determine the following:

- Output current range
- Output current accuracy
- Power consumption for the ATL43xLI-Q1

#### 10.2.5.2.1 Basic Operation

In the configuration shown, the ATL43xLI-Q1 acts as a control component within a feedback loop of the constant current sink. Working with an external passing component such as a BJT, the ATL43xLI-Q1 provides precision current sink with accuracy set by itself and the sense resistor  $R_S$ . The LEDs are lit based on the desired current sink and regulated for accurate brightness and color.

##### 10.2.5.2.1.1 Output Current Range and Accuracy

The output current range of the circuit is determined by the equation shown in the configuration. Keep in mind that the  $V_{REF}$  equals to 2.500 V. When choosing the sense resistor  $R_S$ , it needs to generate 2.500 V for the TL43xLI-Q1 when  $I_O$  reaches the target current. If the overhead voltage of 2.500 V is not acceptable, consider lower voltage reference devices such as the TLV43x-Q1 or TLVH43x-Q1.

The output current accuracy is determined by both the accuracy of the ATL43xLI-Q1 chosen, as well as the accuracy of the sense resistor  $R_S$ . The internal virtual reference voltage of ATL43xLI-Q1 is within the range of  $2.500\text{ V} \pm(0.5\% \text{ or } 1.0\%)$ , depending on which version is being used. Another consideration for the output current accuracy is the temperature coefficient of the ATL43xLI-Q1 and  $R_S$ . Refer to the for the specification of these parameters.

#### 10.2.5.2.2 Power Consumption

For the ATL43xLI-Q1 to properly be used as a control component in this circuit, the minimum operating current needs to be reached. This is accomplished by setting the external biasing resistor in series with the ATL43xLI-Q1.

To achieve lower power consumption, the ATL43xLI-Q1 is used due to its  $65\ \mu\text{A}$  typical minimum cathode current,  $I_{\text{min}}$ .

## 10.2.6 Shunt Regulator/Reference

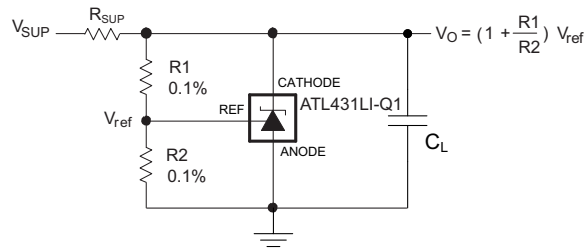


图 26. Shunt Regulator Schematic

### 10.2.6.1 Design Requirements

For this design example, use the parameters listed in 表 1 as the input parameters.

表 3. Design Parameters

DESIGN PARAMETER	EXAMPLE VALUE
Reference Initial Accuracy	1.0%
Supply Voltage	24 V
Cathode Current (I <sub>k</sub> )	5 mA
Output Voltage Level	2.5 V–36 V
Load Capacitance	2 μF
Feedback Resistor Values and Accuracy (R1 and R2)	10 kΩ

### 10.2.6.2 Detailed Design Procedure

When using ATL431LI-Q1 as a shunt regulator, determine the following:

- Input voltage range
- Temperature range
- Total accuracy
- Cathode current
- Reference initial accuracy
- Output capacitance

#### 10.2.6.2.1 Programming Output/Cathode Voltage

To program the cathode voltage to a regulated voltage, a resistive bridge must be shunted between the cathode and anode pins with the mid point tied to the reference pin. This can be seen in 图 26 with R1 and R2 being the resistive bridge. The cathode/output voltage in the shunt regulator configuration can be approximated by the equation shown in 图 26. The cathode voltage can be more accurate, which can be determined by taking in to account the cathode current:

$$V_o = (1 + R1/R2) \times V_{REF} - I_{REF} \times R1 \quad (1)$$

For this equation to be valid, the ATL431LI-Q1 must be fully biased so that it has enough open loop gain to mitigate any gain error. This can be done by meeting the I<sub>min</sub> spec denoted in the [Specifications](#).

### 10.2.6.2.2 Total Accuracy

When programming the output above unity gain ( $V_{KA} = V_{REF}$ ), the ATL431LI-Q1 is susceptible to other errors that can effect the overall accuracy beyond  $V_{REF}$ . These errors include:

- R1 and R2 accuracies
- $V_{I(dev)}$ : Change in reference voltage over temperature
- $\Delta V_{REF} / \Delta V_{KA}$ : Change in reference voltage to the change in cathode voltage
- $|z_{KA}|$ : Dynamic impedance, causing a change in cathode voltage with cathode current

Worst case cathode voltage can be determined taking all of the variables in to account. The [Setting the Shunt Voltage on an Adjustable Shunt Regulator Application Note](#) assists designers in setting the shunt voltage to achieve optimum accuracy for this device.

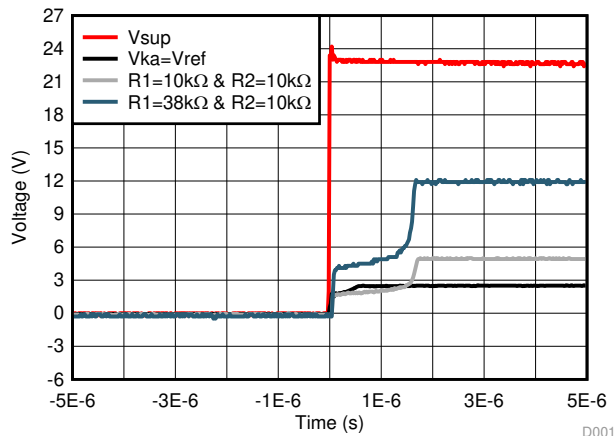
### 10.2.6.2.3 Stability

Though ATL431LI-Q1 is stable with no capacitive load, the device that receives the output voltage of the shunt regulator can present a capacitive load that is within the ATL431LI-Q1 region of stability, shown in [Figure 13](#). Also, designers can use capacitive loads to improve the transient response or for power supply decoupling. When using additional capacitance between Cathode and Anode, see [Figure 13](#). Also, [Understanding Stability Boundary Conditions Charts in TL431, TL432 Data Sheet Application Note](#) provides a deeper understanding of the stability characteristics of this device and aids the user in making the right choices when choosing a load capacitor.

### 10.2.6.2.4 Start-Up Time

As shown in [Figure 27](#), the ATL431LI-Q1 has a fast response up to approximately 2 V and then slowly charges to its programmed value. This is due to the compensation capacitance (shown in [Figure 13](#)) the ATL43xLI-Q1 has to meet its stability criteria. Despite the secondary delay, ATL43xLI-Q1 still has a fast response suitable for many clamp applications.

### 10.2.6.3 Application Curves



**Figure 27. ATL43xLI-Q1 Start-Up Response**



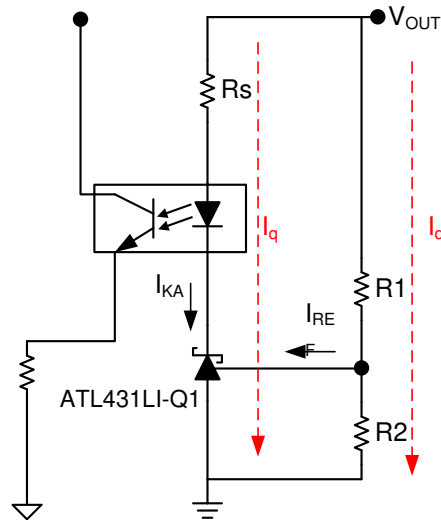


Figure 29. Feedback Quiescent Current

#### 10.2.7.1.1.1 ATL431LI-Q1 Biasing

Figure 29 shows the simplified version of the feedback network. The standby  $I_q$  of the system is dependent on two paths: the ATL431LI-Q1 biasing path and the resistor feedback path. With the given design requirements, the total current through the feedback network cannot exceed 2 mA.

The design goal is to take full advantage of the  $I_{min}$  to set the  $I_{KA}$  of the ATL431LI-Q1. The benefit of the ATL431LI-Q1 is its low  $I_{min}$  of 80  $\mu A$  which allows the  $I_{KA}$  to be lower at a full load condition compared to typical TL431LI-Q1 devices. This helps lower the  $I_{KA}$  at the no-load condition which is higher than the full load condition due to the dynamic changes in the  $I_{KA}$  as the system load varies. The  $I_{KA}$  at no-load,  $I_{OPTNL}$ , is dependent the value of  $R_s$  which is the biasing resistor.  $R_s$  is very application-specific and is dependent on variables such as the CTR of the optocoupler, voltage, and current at no-load. This can be seen in Equation 2. It is possible to lower  $I_{OPTNL}$  to a value of 1.5 mA for a power loss of 30 mW by using an optocoupler with a high CTR.

$$R_s \approx (V_{OUT} - V_{OPTNL} - 2V) / I_{OPTNL}$$

$$V_{OPTNL} = \text{Optocoupler Voltage at No - Load Conditions}$$

$$I_{OPTNL} = \text{Optocoupler Current at No - Load Conditions} \quad (2)$$

#### 10.2.7.1.1.2 Resistor Feedback Network

The feedback resistors set the output voltage of the secondary side and consume the same  $I_q$  at a fixed voltage. The design goal for the feedback resistor path is to minimize the resistor error while maintaining a low  $I_q$ . For this system example, the feedback network path in this design consumes 0.5 mA to allow enough current for ATL431LI-Q1 biasing. The resistors,  $R_1$  and  $R_2$ , are sized based on a 0.5 mA budget for  $I_q$  and  $I_{ref}$ . By using the resistor values from Equation 3 and Equation 4, the total power consumption is 10 mW. This can be further decreased by using larger resistors.

$$R_1 = (V_{OUT} - V_{REF}) / I_{FB}$$

$$R_1 = (20V - 2.5V) / 0.5mA$$

$$R_1 = 35k\Omega \quad (3)$$

$$R_2 = V_{REF} / (I_{FB} - I_{REF})$$

$$R_2 = 2.5V / (0.5mA - 0.4\mu A)$$

$$R_2 = 5.004k\Omega \quad (4)$$

## 10.2.8 Adjustable Reference for Tracking LDO

### 10.2.8.1 Design Requirements

The ATL431LI-Q1 is used as a reference voltage to help regulate a supply voltage off an LDO. By adjusting the cathode voltage, the output voltage of the LDO can vary. The TPS7B4250-Q1 is a voltage-tracking LDO with an adjustable pin which needs a precise reference voltage to change the regulate output voltage.

表 5. Design Parameters

DESIGN PARAMETER	EXAMPLE VALUE
Input Voltage	4 V to 40 V
ADJ Reference Voltage	2.500 V–18 V
Output Voltage	2.500 V–18 V
Output Current Rating	50 mA
Output Capacitor Range	1 $\mu$ F to 50 $\mu$ F
Output Capacitor ESR Range	1 m $\Omega$ to 20 $\Omega$

### 10.2.8.2 Detailed Design Procedure

The goal of this design is to create a precision and stable output stage using an LDO that requires an external voltage reference such as the TPS7B4250-Q1. To begin the design process, the input and desired output voltage range is required. The ATL431LI-Q1 can be adjusted between 2.5 V and 36 V so it covers most of the output voltage rating of TPS7B4250-Q1. For reference voltage under 2.5 V, the TLV431-Q1 voltage reference can be used. The input and output capacitor must also be taken into consideration for decoupling and stability.

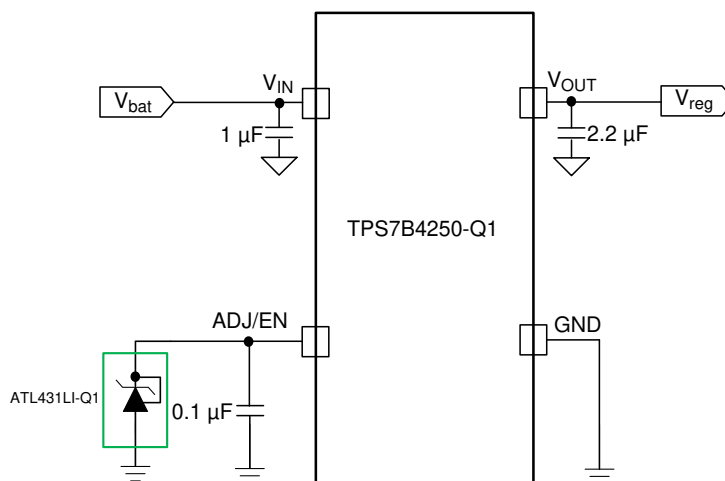


图 30. Feedback Quiescent Current

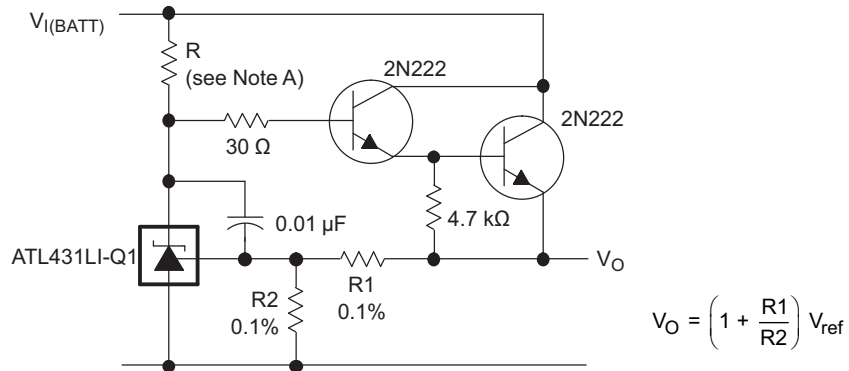
#### 10.2.8.2.1 External Capacitors

An input capacitor, C<sub>I</sub>, is recommended to buffer line influences. Connect the capacitors close to the IC pins.

The output capacitor for the TPS7B4250-Q1 device is required for stability. Without the output capacitor, the regulator oscillates. The actual size and type of the output capacitor can vary based on the application load and temperature range. The effective series resistance (ESR) of the capacitor is also a factor in the IC stability. The worst case is determined at the minimum ambient temperature and maximum load expected. To ensure stability of TPS7B4250-Q1 device, the device requires an output capacitor between 1  $\mu$ F and 50  $\mu$ F with an ESR range between 0.001  $\Omega$  and 20  $\Omega$  that can cover most types of capacitor ESR variation under the recommend operating conditions. As a result, the output capacitor selection is flexible.

The capacitor must also be rated at all ambient temperature expected in the system. To maintain regulator stability down to  $-40^{\circ}\text{C}$ , use a capacitor rated at that temperature.

### 10.3 System Examples



R should provide cathode current  $\geq 80 \mu\text{A}$  to the ATL431LI-Q1 at minimum  $V_{I(BATT)}$ .

FIG 31. Precision High-Current Series Regulator

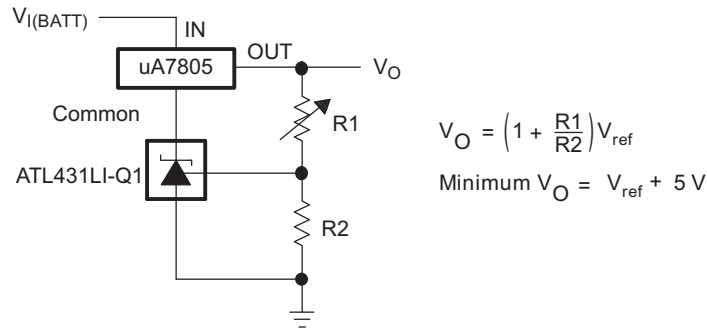


FIG 32. Output Control of a Three-Terminal Fixed Regulator

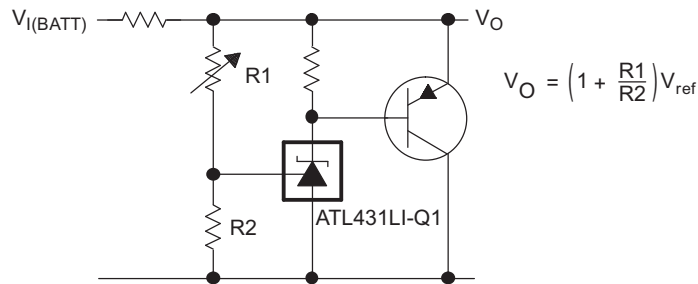
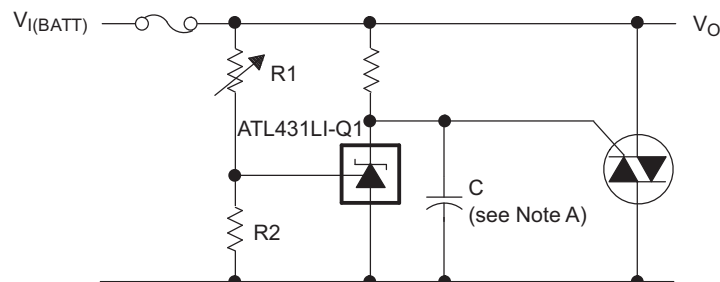


FIG 33. High-Current Shunt Regulator



Refer to the stability boundary conditions in FIG 13 to determine allowable values for C.

FIG 34. Crowbar Circuit



System Examples (continued)

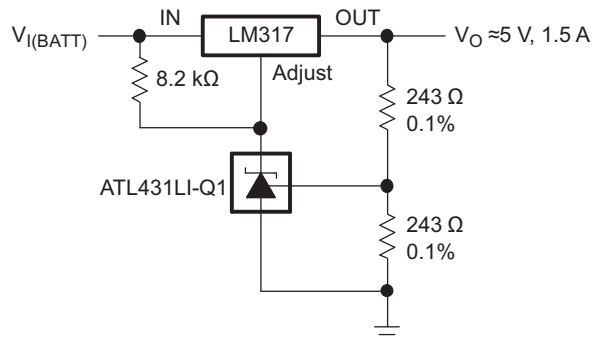
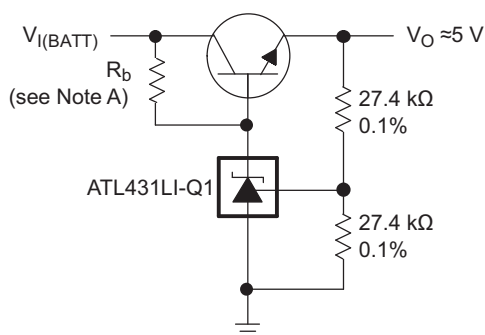


Figure 35. Precision 5-V, 1.5-A Regulator



$R_b$  should provide cathode current  $\geq 80 \mu\text{A}$  to the ATL431LI-Q1.

Figure 36. Efficient 5-V Low-Dropout (LDO) Regulator Configuration

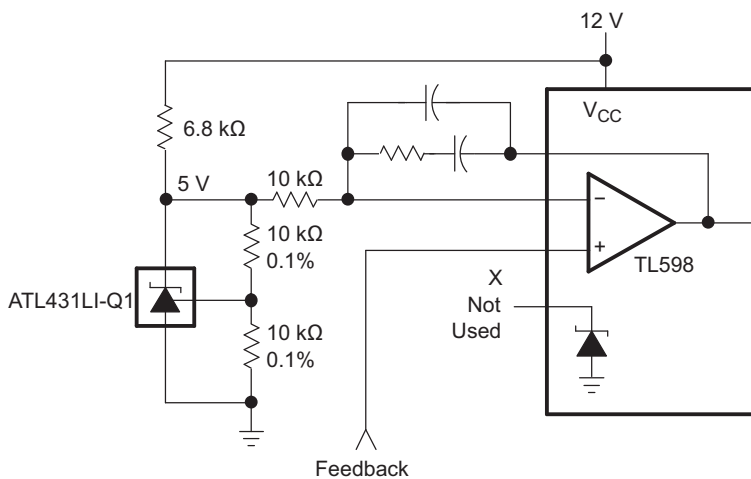
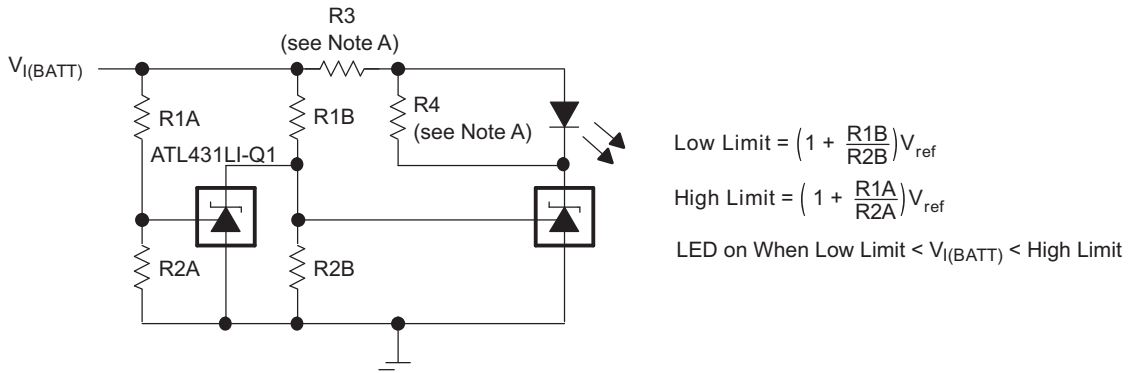


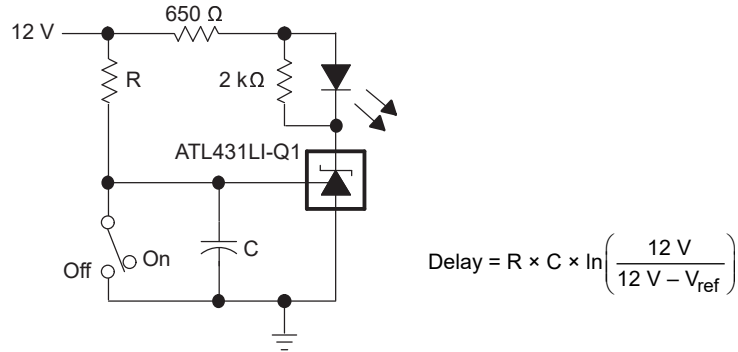
Figure 37. PWM Converter With Reference

System Examples (continued)

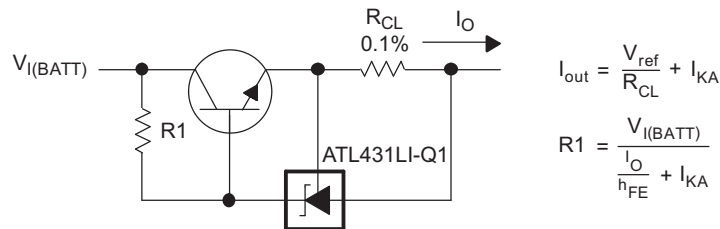


Select R3 and R4 to provide the desired LED intensity and cathode current  $\geq 80 \mu A$  to the ATL431LI-Q1 at the available  $V_{I(BATT)}$ .

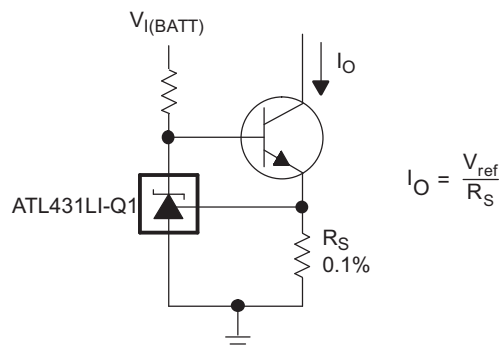
⊠ 38. Voltage Monitor



⊠ 39. Delay Timer



⊠ 40. Precision Current Limiter



⊠ 41. Precision Constant-Current Sink

## 11 Power Supply Recommendations

When using ATL43xLI-Q1 as a Linear Regulator to supply a load, designers typically use a bypass capacitor on the output/cathode pin. When doing this, be sure that the capacitance is within the stability criteria shown in [Figure 13](#).

To not exceed the maximum cathode current, be sure that the supply voltage is current limited. Also, be sure to limit the current being driven into the Ref pin, so you do not exceed its absolute maximum rating.

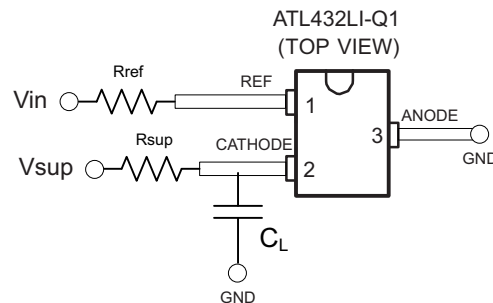
For applications shunting high currents, pay attention to the cathode and anode trace lengths, adjusting the width of the traces to have the proper current density.

## 12 Layout

### 12.1 Layout Guidelines

Bypass capacitors must be placed as close to the part as possible. Current-carrying traces need to have widths appropriate for the amount of current they are carrying; in the case of the ATL43xLI-Q1, these currents are low.

### 12.2 Layout Example



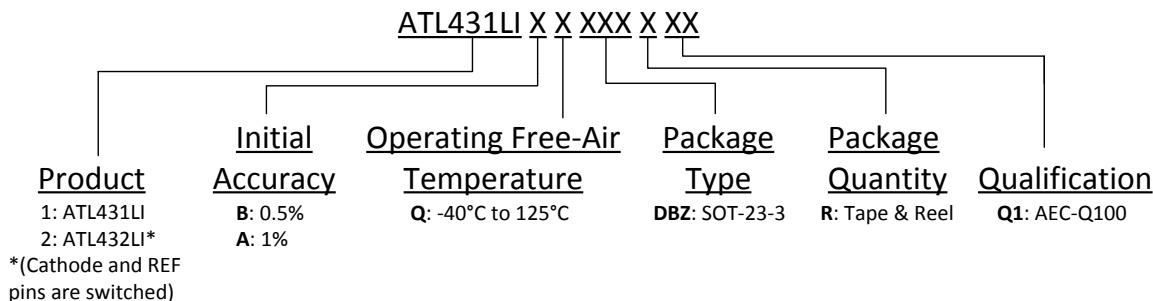
**Figure 42. DBZ Layout Example**

## 13 デバイスおよびドキュメントのサポート

### 13.1 デバイス・サポート

#### 13.1.1 デバイスの項目表記

TI は、ATL43xLI-Q1 ファミリのすべての組み合わせを区別するために、接尾辞と接頭辞を割り当てています。詳細および注文可能な組み合わせについては、「付録: パッケージ・オプション」を参照してください。



### 13.2 ドキュメントのサポート

#### 13.2.1 関連資料

関連資料については、以下を参照してください。

テキサス・インスツルメンツ、[『Setting the Shunt Voltage on an Adjustable Shunt Regulator』](#) (英語)

### 13.3 関連リンク

次の表に、クイック・アクセス・リンクを示します。カテゴリには、技術資料、サポートおよびコミュニティ・リソース、ツールとソフトウェア、およびご注文へのクイック・アクセスが含まれます。

表 6. 関連リンク

製品	プロダクト・フォルダ	ご注文はこちら	技術資料	ツールとソフトウェア	サポートとコミュニティ
ATL431LI-Q1	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>
ATL432LI-Q1	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>	<a href="#">ここをクリック</a>

### 13.4 ドキュメントの更新通知を受け取る方法

ドキュメントの更新についての通知を受け取るには、[ti.com](#)のデバイス製品フォルダを開いてください。右上の「アラートを受け取る」をクリックして登録すると、変更されたすべての製品情報に関するダイジェストを毎週受け取れます。変更の詳細については、修正されたドキュメントに含まれている改訂履歴をご覧ください。

### 13.5 サポート・リソース

TI E2E™ support forums are an engineer's go-to source for fast, verified answers and design help — straight from the experts. Search existing answers or ask your own question to get the quick design help you need.

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### 13.6 商標

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### 13.7 静電気放電に関する注意事項



すべての集積回路は、適切なESD保護方法を用いて、取扱いと保存を行うようにして下さい。

静電気放電はわずかな性能の低下から完全なデバイスの故障に至るまで、様々な損傷を与えます。高精度の集積回路は、損傷に対して敏感であり、極めてわずかなパラメータの変化により、デバイスに規定された仕様に適合しなくなる場合があります。

### 13.8 Glossary

[SLYZ022](#) — *TI Glossary*.

This glossary lists and explains terms, acronyms, and definitions.

## 14 メカニカル、パッケージ、および注文情報

以降のページには、メカニカル、パッケージ、および注文に関する情報が記載されています。この情報は、そのデバイスについて利用可能な最新のデータです。このデータは予告なく変更されることがあり、ドキュメントが改訂される場合もあります。本データシートのブラウザ版を使用されている場合は、画面左側の説明をご覧ください。

**PACKAGING INFORMATION**

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
ATL431LIAQDBZRQ1	ACTIVE	SOT-23	DBZ	3	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	22XP	<a href="#">Samples</a>
ATL431LIBQDBZRQ1	ACTIVE	SOT-23	DBZ	3	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	22ZP	<a href="#">Samples</a>
ATL432LIAQDBZRQ1	ACTIVE	SOT-23	DBZ	3	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	23AP	<a href="#">Samples</a>
ATL432LIBQDBZRQ1	ACTIVE	SOT-23	DBZ	3	3000	RoHS & Green	NIPDAU	Level-1-260C-UNLIM	-40 to 125	23BP	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSELETE:** TI has discontinued the production of the device.

(2) **RoHS:** TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".

**RoHS Exempt:** TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.

**Green:** TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

(3) MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

(5) Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "-" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

(6) Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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## TAPE AND REEL INFORMATION



### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
ATL431LIAQDBZRQ1	SOT-23	DBZ	3	3000	178.0	9.0	3.15	2.77	1.22	4.0	8.0	Q3
ATL431LIBQDBZRQ1	SOT-23	DBZ	3	3000	178.0	9.0	3.15	2.77	1.22	4.0	8.0	Q3
ATL432LIAQDBZRQ1	SOT-23	DBZ	3	3000	178.0	9.0	3.15	2.77	1.22	4.0	8.0	Q3
ATL432LIBQDBZRQ1	SOT-23	DBZ	3	3000	178.0	9.0	3.15	2.77	1.22	4.0	8.0	Q3



## TAPE AND REEL BOX DIMENSIONS



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
ATL431LIAQDBZRQ1	SOT-23	DBZ	3	3000	180.0	180.0	18.0
ATL431LIBQDBZRQ1	SOT-23	DBZ	3	3000	180.0	180.0	18.0
ATL432LIAQDBZRQ1	SOT-23	DBZ	3	3000	180.0	180.0	18.0
ATL432LIBQDBZRQ1	SOT-23	DBZ	3	3000	180.0	180.0	18.0

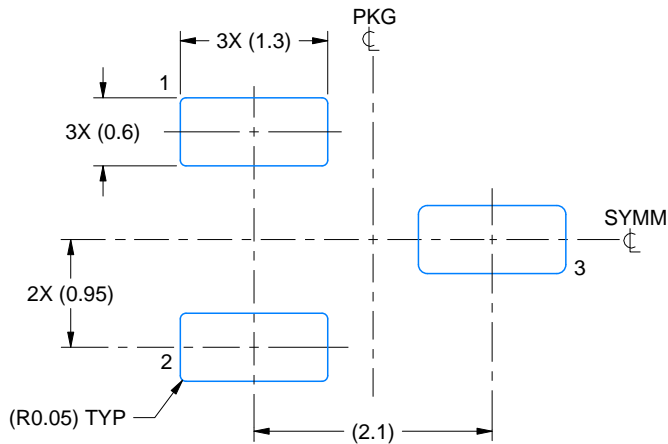


# EXAMPLE BOARD LAYOUT

DBZ0003A

SOT-23 - 1.12 mm max height

SMALL OUTLINE TRANSISTOR



LAND PATTERN EXAMPLE  
SCALE:15X



SOLDER MASK DETAILS

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NOTES: (continued)

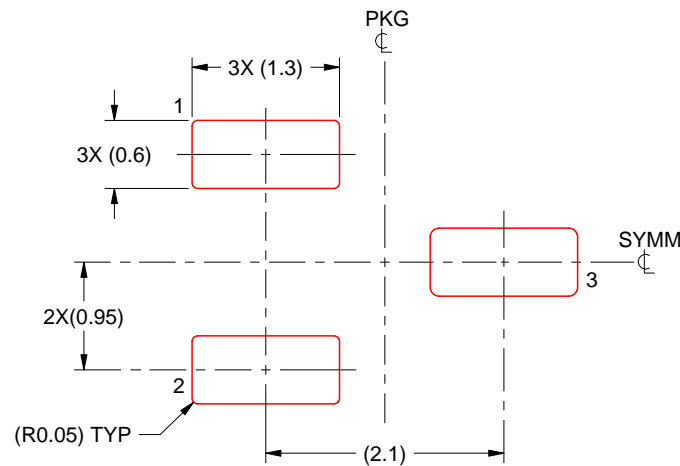
5. Publication IPC-7351 may have alternate designs.
6. Solder mask tolerances between and around signal pads can vary based on board fabrication site.

# EXAMPLE STENCIL DESIGN

DBZ0003A

SOT-23 - 1.12 mm max height

SMALL OUTLINE TRANSISTOR



SOLDER PASTE EXAMPLE  
BASED ON 0.125 THICK STENCIL  
SCALE:15X

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NOTES: (continued)

7. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
8. Board assembly site may have different recommendations for stencil design.

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